# Technical Memorandum 

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Project: City of Reedsport Rail Crossing Study and Refinement Plan
Subject: Tech Memo \#5: Future Land Use and Transportation Conditions

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## INTRODUCTION

This memorandum summarizes future (no-build) transportation system conditions within the study area for the Reedsport Rail Crossing Study and Refinement Plan, including future gaps, deficiencies, and needs to accommodate future growth. The information provided in this memorandum reflects planned improvements identified in State and local planning documents as well as forecast traffic volumes developed for the study area. The future gaps, deficiencies, and needs identified in this memorandum will serve as the basis for developing transportation system alternatives and improvement projects for the Reedsport Rail Crossing Study and Refinement Plan.

## PLANNED IMPROVEMENTS

This section summarizes planned improvements identified in the Oregon Department of Transportation (ODOT) Statewide Transportation Improvement Program (STIP) and City of Reedsport (City) Capital Improvement Program (CIP). One expected outcome of the Reedsport Rail Crossing Study and Refinement Plan is the identification of projects for inclusion in updated versions of the ODOT STIP and City CIP.

## Statewide Transportation Improvement Program

The Statewide Transportation Improvement Program (STIP) is the ODOT's 4-year capital improvement program for State and federally funded projects. The Oregon Transportation Commission (OTC) and ODOT develop the STIP in coordination with a wide range of stakeholders, including local jurisdictions and the public. The OTC allocates funding among the following categories:

- Fix-it programs fund projects that fix or preserve the state's transportation system, including bridges, pavement, culverts, traffic signals, and others.
- Enhance-it programs fund projects that enhance or expand the transportation system. These are typically high-priority projects from State and local transportation plans, such as the Reedsport TSP.
- Safety programs reduce fatalities and injuries on Oregon roads. This includes the All Roads Transportation Safety (ARTS) program, which includes projects on State highways and local roads.
- Non-highway programs fund bicycle and pedestrian projects and public transportation.
- Local government programs direct funding to local governments so they can fund projects.

The current STIP (2021-2024) includes two projects in the Reedsport area and the draft STIP (2024-2027) includes one project. Table 1 summarizes projects from the current and draft STIP.

Table 1. ODOT 2021-2024 and Draft 2024-2027 STIP Projects for Reedsport

| Key | Project Name | Projects | Work <br> type | Status | Project Tołal |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Current STIP (2021-2024) |  |  |  |  |  |
| 20153 | US 101/OR 38: Variable Message Signs | Replace existing hazard warning system with LID-based variable message (VMS) system to increase visibility to the traveling public | OP-ITS | Construction contract complete | \$2,022,870.51 |
| 22387 | US 101/OR 38 Curb Ramps | Construct curb ramps to meet compliance with American with Disabilities Act (ADA) standards | ADAP | Project under construction | \$6,192,472.36 |
| Draft STIP (2024-2027) |  |  |  |  |  |
| 22977 | US 101: Washington State Line to California State Line | Install National Electric Vehicle Infrastructure (NEVI) fast-charging stations at 50-mile internals along US 101 | Electric | Project scheduled for construction | \$6,281,000 |

The project(s) shown in Table 1 will be considered in the future (no-build) traffic conditions analysis; however, they are not expected to directly impact study intersection operations.

## Reedsport Capital Improvement Plan

The City CIP is a short-range plan for capital improvement projects and funding sources in the City. Table 2 lists relevant project from the 2023-2027 CIP in the study area.

Table 2. City of Reedsport 2023-2027 Capital Improvement Projects

| Fiscal <br> Year | Fund |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 2023 | 150 | Grojects | Estimated Cost | Funding Source |
| $2023-2027$ | 002 | Americans with Disabilities Act Upgrades | $\$ 50,000$ | None listed |


| 2026 | 002 | Winchester Ave. 2nd Phase Paving | $\$ 150,000$ | Pending SCA Grant |
| :---: | :---: | :--- | :---: | :---: |
| 2024 | $005 / 150$ | Levee Repairs and Upgrades | $\$ 5,600,000$ | Pending grant |

The project(s) shown in Table 2 were considered in the future (no-build) traffic conditions analysis summarized below and will be further evaluated in the alternatives analysis.

## FUTURE TRAFFIC VOLUMES

Forecast traffic volumes were developed for the study intersections based on the existing traffic counts and an assessment of data from the Statewide Integrated Model (SWIM), ODOT's Future Volume Tables, and Automatic Traffic Recorders (ATRs) located along US 101 and OR 38 as indicated below.

- The SWIM provides base and forecast year traffic volume projections for the study area that reflect anticipated land use changes and planned transportation improvements. The model is up-to-date and readily available with base year 2019 and future year 2045 traffic volume projections. Based on the data, traffic volumes along US 101 and OR 38 are expected to grow by approximately $1.0 \%$ per year through the planning horizon.
- ODOT's Future Volume Tables also provide base and forecast year traffic volume projections for the study area. The model provides base year 2021 and future year 2041 traffic volume projections. Based on the data, traffic volumes are expected to grow by approximately $0.05 \%$ per year along US 101 and $0.10 \%$ per year along OR 38 through the planning horizon.
- ATRs are located in select locations throughout the State highway system and collect traffic data 24hours a day, 365 days a year. Data from two ATRs located near the study area were analyzed to determine potential growth rates for the study area. The Scottsburg ATR (\#10-003) located on OR 38 approximately 7.08 miles east of Scottsburg West Roads shows traffic volume growth of approximately $1.02 \%$ per year over the last 10 years, excluding year 2020 volumes. The Lakeside ATR (\#06-001) located on US 101 approximately 1.09 miles south of the Douglas and Coos County line shows traffic volume growth of approximately $0.50 \%$ per year over the last 10 years, excluding year 2020 volumes.

Based on an assessment of the growth rates described above, the growth rates from the SWIM were applied to existing traffic volumes along US 101 and OR 38 to estimate growth in regional traffic volumes. The SWIM annual growth rate was also applied to the local side street movements in the study area to yield a more conservative future traffic analysis.

## MOTOR VEHICLE TRANSPORTATION ANALYSIS

## Intersection Operations Analysis

The intersection operations analysis was conducted using PTV Vistro 2022, which is a software tool designed to assist with operations analyses in accordance with Highway Capacity Manual (HCM) methodologies. The analysis results include level-of-service (LOS), delay (del), and volume-to-capacity ( $\mathrm{v} / \mathrm{c}$ ) ratios at all intersections, regardless of jurisdiction. The LOS, del, and v/c ratios are reported for the overall intersection at signalized intersections and the critical movement at unsignalized intersections in accordance with the methodologies outlined in ODOT's Analysis Procedures Manual (APM).p

Table 3 and Figure 1 summarize the results of the intersection operations analysis and compares the results to the applicable mobility standards and targets, which were presented in Technical Memorandum \#3: Analysis Methodology and Assumptions. Values shown in bold exceed their applicable mobility standard/ target. Attachment A to this memorandum contains the year 2045 traffic conditions worksheets.

Table 3. Year 2045 Intersection Operations, Weekday PM Peak Hour

| Map ID | Intersection | Control Type | Mobility <br> Standard/Targe ${ }^{\dagger 1}$ | Intersection Operations |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | CM | LOS 2 | Del3 | $\mathrm{v} / \mathrm{c}^{4}$ |
| 1 | US 101/OR $38{ }^{1}$ | Signal | $\mathrm{v} / \mathrm{c}=0.85$ | WB/L | C | 31.8 | 1.0 |
| 2 | W. Railroad Avenue/OR 38 | TWSC | $\mathrm{v} / \mathrm{c}=0.85 / 0.95$ | NB/L | C | 16.1 | 0.02 |
| 3 | E. Railroad Avenue/OR 38 | TWSC | $\mathrm{v} / \mathrm{c}=0.85 / 0.95$ | NB/T | C | 15.8 | 0.01 |
| 4 | N. 6th Street/OR 38 | TWSC | $\mathrm{v} / \mathrm{c}=0.85 / 0.95$ | NB/L | C | 15.4 | 0.04 |
| 5 | OR 38/Riverfront Way-Winchester Avenue | TWSC | $\mathrm{V} / \mathrm{C}=0.85 / 0.95$ | NB/L | C | 19.5 | 0.14 |
| 6 | US 101/Winchester Avenue | Signal | $v / \mathrm{c}=0.85$ | WB/L | B | 11.0 | 0.55 |
| 7 | W. Railroad Avenue/Winchester Avenue | TWSC | LOS D | NB/L | B | 10.5 | 0.03 |
| 8 | Elm Avenue/Winchester Avenue | TWSC | LOS D | NB/L | B | 10.2 | 0.02 |
| 9 | E. Railroad Avenue/Winchester Avenue | TWSC | LOS D | NB/L | B | 11.0 | 0.02 |
| 10 | South 6th Street/Winchester Avenue | TWSC | LOS D | SB/T | B | 10.5 | 0.01 |

${ }^{1}$ State highway $\mathrm{v} / \mathrm{c}$ ratio/side-street $\mathrm{v} / \mathrm{c}$ ratio.
${ }^{2}$ LOS = Intersection LOS (signal); CM LOS (TWSC).
${ }^{3}$ Delay = Intersection average vehicle delay (signal); CM vehicle delay (TWSC).
${ }^{4} \mathrm{v} / \mathrm{c}=$ Intersection $\mathrm{v} / \mathrm{c}$ (signal); CM v/c (TWSC).
$C M=$ critical movement; Del = delay; L = left; $T$ = through; LOS = level of service; $N B=$ northbound; TWSC = two-way stopcontrol; $S B=$ southbound; $W B=$ westbound; $\mathrm{v} / \mathrm{c}=$ volume-to-capacity.

As shown in Table 3 and Figure 1, all study intersections are forecast to meet their applicable mobility standards and targets except the US 101/OR 38 intersection, which is forecast to operate at an intersection v/c of 1.0 in the year 2045. The westbound left-through movement is expected to be the critical movement and is forecast to operate at a v/c of 0.95 .

The Reedsport Transportation System Plan (TSP) projects the US 101/OR 38 intersection to meet mobility targets in the planning horizon year of 2025. The Reedsport Waterfront and Downtown Plan forecasted the US 101/OR 38 intersection to meet mobility targets and operate at a v/c of 0.84 in 2033. The additional 12 years of growth at the intersections to 2045 is forecasted to bring the intersection to capacity at a v/c of 1.0.

## Queueing Analysis

A queuing analysis during non-train events was conducted at the signalized study intersections using PTV Vistro 2022. Table 4 summarizes the year 2045 95th percentile queues during the weekday PM peak hour and indicates if existing storage can accommodate the queues. The vehicle queues and storage lengths were rounded up to the nearest 25 feet. The storage lengths reflect the striped storage for each movement at the intersections or the distance to the upstream intersection. Values shown in bold exceed their available storage. Unsignalized intersection queues were also analyzed and were found to be less than one vehicle length during the peak hour. Attachment A contains the queuing analysis worksheets.

[^0]Table 4. Queueing Summary, Year 2045 Weekday PM Peak Hour

| Map <br> ID | Intersection | Movement | Storage Length <br> (feet) | 95th Percentile <br> Queve (feet) | Adequate? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | US 101/ OR 38 | EBTL | 200 | 50 | Yes |

$E B=$ eastbound; $L=$ left; $\mathrm{NB}=$ northbound; $\mathrm{SB}=$ southbound; $\mathrm{R}=$ right; $\mathrm{T}=$ through; $\mathrm{WB}=$ westbound.
As shown in Table 4., the striped storage lengths at the signalized study intersections are currently adequate to accommodate the 95th percentile queues, except the westbound through-left movement, which is forecast to have a queue extend south of Myrtle Avenue during the weekday PM peak hour.

Figure 1. Year 2045 Traffic Conditions, Weekday PM Peak Hour


## RAIL

The CBRL provides freight service to industrial customers in and around Coos Bay and Coquille via interchange connections with the Union Pacific Railroad in Eugene, approximately 120 railroad miles to the north and east.

## Future Operations

Future operations on the CBRL would increase rail traffic through Reedsport by way of containerized rail traffic moving to/from an international container port being planned within Coos Bay. The proposed container facility will be designed to accommodate 1.2 million Twenty-foot Equivalent Unit (TEU) containers per year, which equates to approximately 600,000 containers per year. Depending upon the operational length of trains on the CBRL, as well as several other factors documented in Tech Memo \#3: Analysis Methodology and Assumptions, the number of trains could vary from 10 to 12 intermodal trains per day ( 4,000 to 5,000 feet per train, respectively). The operational length of the trains will be limited largely by the grades and curvature along the rail line after improvements, all of which have yet to be finalized.

Based on CBRL train characteristics and potential operational speed restrictions within Reedsport, the following train analysis assumptions were used for analysis and are summarized in Table 5.

Table 5. Train Characteristics Assumptions

| Train | Length (ft) | Speed (mph) | Crossing Time (min) |
| :--- | :---: | :---: | :---: |
| Intermodal | 4,000 | 25 | 3 |
| Intermodal (current speed restrictions) | 4,000 | 10 | 5 |
| Mixed Freight Traffic | 1,500 | 25 | 2 |

The goal for operational speeds for the improved rail line was stated by CBRL as 40 mph ; however, it is possible that the swing span bridge across the Umpqua River could still present an operational speed restriction within Reedsport even after capital improvements. Based upon this, the crossings were analyzed under an operational speed of 25 mph within Reedsport and existing 10 mph speed restrictions for a conservative approach with respect to grade crossing blockages by passing trains.

## Rail Crossing Controls and Configurations

Future rail crossing controls and configurations have not been identified. The two at-grade rail crossings in the City of Reedsport on OR 38 and Winchester Avenue are anticipated to remain under this no-build analysis documented herein.

## Train Event Considerations

Impacts of train events at the railroad crossings on OR 38 and Winchester Avenue were evaluated for the future operations on the Coos Bay Rail Line (CBRL) conditions. Projected queueing outcomes during intermodal and mixed freight train events were used to estimate queueing. Queues were calculated using the crossing volumes and heavy vehicle percentages, including the total eastbound and total westbound approaches. For the analysis it was assumed a heavy vehicle is 75 feet and a passenger car is 25 feet. Train
event assumptions are detailed above and in Technical Memorandum \#3: Analysis Methodology and Assumptions.

The 95th percentile queue lengths shown quantify those lengths that have a 5 percent probability of being exceeded during a train crossing. These were calculated by applying a Poisson distribution to the expected number of vehicle arrivals during each train crossing time and summing the associated probability for each number of arrivals, starting at zero vehicles, until a total probability of $95 \%$ was attained. The 95th percentile queue lengths are shown in Table 6 and Figure 2. Values shown in bold exceed their available storage.

Table 6. Train Event Year 2045 95th Percentile Queueing

| Crossing | Approach | Storage Length (feet) | 95th Percentile Queves (feet) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Existing | Intermodal ał $25 \mathrm{mph} /$ Intermodal at $10 \mathrm{mph} /$ Mixed Freight at 25 mph | Exceeds Słorage? |
| OR 38 | Eastbound | $140^{1}$ | 525 | 625/975/450 | Yes |
|  | Westbound | 1502 | 600 | 700/1100/500 | Yes |
| Winchester Avenue | Eastbound | $130^{1}$ | 225 | 275/425/200 | Yes |
|  | Westbound | $10{ }^{2}$ | 250 | 300/450/200 | Yes |

${ }^{1}$ Distance to W. Railroad Avenue.
${ }^{2}$ Distance to E. Railroad Avenue.
The 95th percentile queve lengths are anticipated to still exceed storage for eastbound and westbound movements on OR 38 and Winchester Avenue. During a future train event, OR 38 eastbound traffic is expected to queve west of Laurel Avenue, and westbound traffic is expected to queue east of N. 6th Street during an intermodal train event. On Winchester Avenue, the eastbound traffic is expected to queue west of W. Railroad Avenue, and westbound traffic is expected to queve east of E. Railroad Avenue during an intermodal train event. During a future mixed freight train event, queues are expected to be less than the existing train event as future trains are anticipated to operate at $25 \mathrm{mph}, 15 \mathrm{mph}$ more than existing conditions.

During a future intermodal train event with existing speed restrictions in place, OR 38 eastbound traffic is expected to queue west of Myrtle Avenue, and westbound traffic is expected to queue east of N. 5th Street. On Winchester Avenue, the eastbound traffic is expected to queue west of W. Railroad Avenue, and westbound traffic is expected to queve east of E. Railroad Avenue during an intermodal train event with existing speed restrictions in place. In an event with a train length exceeding 4, 100 feet at 10 mph , the OR 38 eastbound traffic is expected to queue to US 101. Attachment $B$ contains the train event queuing calculations.

Figure 2. Train Event Queue Lengths


## FUTURE DEFICIENCIES AND NEEDS

This memorandum identified the following future deficiencies and needs:

- Capacity - Under future year 2045 conditions, the US 101/OR 38 intersection is expected to exceed mobility targets and operate at capacity ( $\mathrm{v} / \mathrm{c}=1.0$ ) in the weekday PM peak hour.
- Queue storage - Under future year 2045 conditions, westbound through-left queueing at the US 101/OR 38 intersection is expected to exceed striped storage in the weekday PM peak hour.
- Train event queue storage - Train events are likely to cause queues on OR 38 and Winchester Avenue that exceed the eastbound and westbound approach storage length today and in the future. During a 4,100-foot or greater train event at 10 mph with current Umpqua swing span speed restrictions, eastbound OR 38 queues would be expected to extend to US 101.


## ATTACHMENTS

A. Future Traffic Conditions Worksheets
B. Future Train Event Queueing Calculations

## Attachment A: Future Traffic Conditions Worksheets

 Intersection 1: US 101 / OR 38Control Type: Analysis Method: Analysis Period:

Signalized
HCM 6th Edition 15 minutes

| Delay (sec / veh): | 31.8 |
| :---: | :---: |
| Level Of Service: | C |
| Volume to Capacity $(\mathrm{v} / \mathrm{c}):$ | 1.004 |

Intersection Setup

| Name | US 101 |  |  | US 101 |  |  | Port Dock Rd |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $7 \\| F$ |  |  | $71 F$ |  |  | $\uparrow$ |  |  | $\uparrow \Gamma$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Entry Pocket Length [ft] | 150.00 | 100.00 | 100.00 | 225.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 320.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 49.21 |
| Speed [mph] | 30.00 |  |  | 30.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Curb Present | Yes |  |  | No |  |  | Yes |  |  | No |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | No |  |  |

Volumes

| Name | US 101 |  |  | US 101 |  |  | Port Dock Rd |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 21 | 292 | 258 | 50 | 333 | 17 | 16 | 10 | 33 | 288 | 6 | 57 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 18.00 | 9.00 | 5.00 | 2.00 | 6.00 | 0.00 | 0.00 | 50.00 | 11.00 | 9.00 | 20.00 | 0.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 21 | 292 | 258 | 50 | 333 | 17 | 16 | 10 | 33 | 288 | 6 | 57 |
| Peak Hour Factor | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 6 | 79 | 70 | 14 | 90 | 5 | 4 | 3 | 9 | 78 | 2 | 15 |
| Total Analysis Volume [veh/h] | 23 | 317 | 280 | 54 | 362 | 18 | 17 | 11 | 36 | 313 | 7 | 62 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| v_do, Outbound Pedestrian Volume crossing | 0 |  |  | 0 |  |  | 1 |  |  | 0 |  |  |
| v_di, Inbound Pedestrian Volume crossing m | 1 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| v_co, Outbound Pedestrian Volume crossing | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| v_ci, Inbound Pedestrian Volume crossing rii | i 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| v_ab, Corner Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 1 |  |  | 1 |  |  | 1 |  |  | 0 |  |  |

27003 Reedsport Rail Crossing Study
HCM 6th Edition
Version 2022 (SP 0-2)
Year 2045 Traffic Conditions
Weekday PM Peak Hour
Intersection Settings

| Located in CBD |  |
| :---: | :---: |
| Signal Coordination Group |  |
| Cycle Length [s] |  |
| Coordination Type |  |
| Actuation Type | Free Running |
| Offset [s] | Fully actuated |
| Offset Reference | 0.0 |
| Permissive Mode | Lead Green - Beginning of First Green |
| Lost time [s] | SingleBand |
| 12.00 |  |

Phasing \& Timing

| Control Type | ProtPer | Permiss | Permiss | ProtPer | Permiss | Permiss | Permiss | Permiss | Permiss | Permiss | Permiss | Permiss |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal Group | 1 | 6 | 0 | 5 | 2 | 0 | 0 | 8 | 0 | 0 | 4 | 0 |
| Auxiliary Signal Groups |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead / Lag | Lag | - | - | Lag | - | - | - | - | - | - | - | - |
| Minimum Green [s] | 3 | 10 | 0 | 3 | 10 | 0 | 0 | 5 | 0 | 0 | 7 | 0 |
| Maximum Green [s] | 15 | 45 | 0 | 15 | 45 | 0 | 0 | 35 | 0 | 0 | 35 | 0 |
| Amber [s] | 3.5 | 3.8 | 0.0 | 3.5 | 3.8 | 0.0 | 0.0 | 3.5 | 0.0 | 0.0 | 3.8 | 0.0 |
| All red [s] | 1.8 | 1.0 | 0.0 | 1.8 | 1.5 | 0.0 | 0.0 | 1.8 | 0.0 | 0.0 | 2.0 | 0.0 |
| Split [s] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Vehicle Extension [s] | 2.5 | 4.5 | 0.0 | 2.5 | 4.5 | 0.0 | 0.0 | 2.5 | 0.0 | 0.0 | 2.5 | 0.0 |
| Walk [s] | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 0 | 0 |
| Pedestrian Clearance [s] | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 20 | 0 | 0 | 0 | 0 |
| Delayed Vehicle Green [s] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Rest In Walk |  | No |  |  | No |  |  | No |  |  | No |  |
| 11, Start-Up Lost Time [s] | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 |
| 12, Clearance Lost Time [s] | 3.3 | 2.8 | 0.0 | 3.3 | 3.3 | 0.0 | 0.0 | 3.3 | 0.0 | 0.0 | 3.8 | 0.0 |
| Minimum Recall | No | Yes |  | No | Yes |  |  | No |  |  | No |  |
| Maximum Recall | No | No |  | No | No |  |  | No |  |  | No |  |
| Pedestrian Recall | No | No |  | No | No |  |  | No |  |  | No |  |
| Detector Location [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector Length [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| I, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

## Exclusive Pedestrian Phase

| Pedestrian Signal Group |  |
| :---: | :--- |
| Pedestrian Walk [s] | 0 |
| Pedestrian Clearance [s] | 0 |

## Lane Group Calculations

| Lane Group | L | C | C | R | L | C | C | C | C | R |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C, Cycle Length [s] | 69 | 69 | 69 | 69 | 69 | 69 | 69 | 69 | 69 | 69 |
| L, Total Lost Time per Cycle [s] | 5.05 | 4.80 | 4.80 | 4.80 | 5.30 | 5.30 | 5.30 | 5.30 | 5.80 | 5.80 |
| I1_p, Permitted Start-Up Lost Time [s] | 2.00 | 0.00 | 0.00 | 0.00 | 2.00 | 0.00 | 0.00 | 2.00 | 2.00 | 0.00 |
| 12, Clearance Lost Time [s] | 0.00 | 2.80 | 2.80 | 2.80 | 0.00 | 3.30 | 3.30 | 0.00 | 3.80 | 3.80 |
| g_i, Effective Green Time [s] | 23 | 16 | 16 | 16 | 23 | 17 | 17 | 35 | 35 | 35 |
| $\mathrm{g} / \mathrm{C}$, Green / Cycle | 0.33 | 0.23 | 0.23 | 0.23 | 0.33 | 0.24 | 0.24 | 0.51 | 0.51 | 0.51 |
| (v / s)_i Volume / Saturation Flow Rate | 0.02 | 0.12 | 0.12 | 0.12 | 0.04 | 0.11 | 0.11 | 0.27 | 0.70 | 0.04 |
| s , saturation flow rate [veh/h] | 1120 | 1765 | 1614 | 1518 | 1209 | 1810 | 1776 | 233 | 456 | 1615 |
| c, Capacity [veh/h] | 325 | 402 | 368 | 346 | 344 | 438 | 430 | 87 | 333 | 816 |
| d1, Uniform Delay [s] | 22.17 | 23.44 | 23.50 | 23.50 | 23.93 | 22.24 | 22.26 | 14.22 | 21.98 | 8.81 |
| k, delay calibration | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.08 | 0.19 | 0.08 | 0.50 | 0.08 |
| I, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 0.16 | 1.81 | 2.07 | 2.30 | 0.36 | 0.51 | 1.21 | 8.62 | 40.07 | 0.03 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp , platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

Lane Group Results

| X, volume / capacity | 0.07 | 0.52 | 0.54 | 0.55 | 0.16 | 0.44 | 0.44 | 0.74 | 0.96 | 0.08 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 22.33 | 25.25 | 25.57 | 25.80 | 24.29 | 22.75 | 23.47 | 22.84 | 62.05 | 8.83 |
| Lane Group LOS | C | C | C | C | C | C | C | C | E | A |
| Critical Lane Group | No | No | No | Yes | Yes | No | No | No | Yes | No |
| 50th-Percentile Queue Length [veh/ln] | 0.25 | 3.07 | 2.90 | 2.80 | 0.59 | 2.56 | 2.62 | 0.67 | 9.02 | 0.45 |
| 50th-Percentile Queue Length [ft/ln] | 6.14 | 76.87 | 72.55 | 70.09 | 14.68 | 64.01 | 65.41 | 16.69 | 225.52 | 11.24 |
| 95th-Percentile Queue Length [veh/ln] | 0.44 | 5.53 | 5.22 | 5.05 | 1.06 | 4.61 | 4.71 | 1.20 | 13.95 | 0.81 |
| 95th-Percentile Queue Length [ft/ln] | 11.06 | 138.3 | 130.5 | 126.1 | 26.42 | 115.21 | 117.74 | 30.03 | 348.67 | 20.23 |

Version 2022 (SP 0-2)
Year 2045 Traffic Conditions
Weekday PM Peak Hour
Movement, Approach, \& Intersection Results

| d_M, Delay for Movement [s/veh] | 22.33 | 25.36 | 25.73 | 24.29 | 23.09 | 23.47 | 22.84 | 22.84 | 22.84 | 62.05 | 62.05 | 8.83 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | C | C | C | C | C | C | C | C | C | E | E | A |
| d_A, Approach Delay [s/veh] | 25.41 |  |  | 23.25 |  |  | 22.84 |  |  | 53.42 |  |  |
| Approach LOS | C |  |  | C |  |  | C |  |  | D |  |  |
| d_l, Intersection Delay [s/veh] | 31.81 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 1.004 |  |  |  |  |  |  |  |  |  |  |  |

## Other Modes

| g_Walk,mi, Effective Walk Time [s] | 11.0 | -5.8 | 11.0 | 0.0 |
| :---: | :---: | :---: | :---: | :---: |
| M_corner, Corner Circulation Area [ft'/ped] | 0.00 | 0.00 | 0.00 | 0.00 |
| M_CW, Crosswalk Circulation Area [fti/ped] | 7991.55 | 0.00 | 0.00 | 0.00 |
| d_p, Pedestrian Delay [s] | 24.52 | 40.69 | 24.52 | 0.00 |
| I_p,int, Pedestrian LOS Score for Intersectiqn | 3.100 | 2.555 | 1.775 | 0.000 |
| Crosswalk LOS | C | B | A | F |
| s_b, Saturation Flow Rate of the bicycle land | 2000 | 2000 | 2000 | 2000 |
| c_b, Capacity of the bicycle lane [bicycles/h] | 1299 | 1299 | 1010 | 1010 |
| d_b, Bicycle Delay [s] | 4.26 | 4.26 | 8.49 | 8.49 |
| I_b,int, Bicycle LOS Score for Intersection | 2.071 | 1.918 | 1.665 | 2.190 |
| Bicycle LOS | B | A | A | B |

Sequence

| Ring 1 | 1 | 2 | - | 4 | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ring 2 | 5 | 6 | - | 8 | - | - | - | - | - | - | - | - | - | - | - | - |
| Ring 3 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Ring 4 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |



## Generated with PTV VISTRO

27003 Reedsport Rail Crossing Study
HCM 6th Edition
Version 2022 (SP 0-2)
Year 2045 Traffic Conditions
Weekday PM Peak Hour
Intersection Level Of Service Report
Intersection 2: OR 38 / W Railroad Ave

Control Type: Analysis Method: Analysis Period:

Two-way stop
HCM 6th Edition
15 minutes

Delay (sec / veh):
Level Of Service:
Volume to Capacity ( $\mathrm{v} / \mathrm{c}$ ):
Volume to Capacity ( $\mathrm{v} / \mathrm{c}$ ):
16.1

C
0.015

Intersection Setup

| Name | W Railroad Ave |  |  | W Railroad Ave |  |  | OR 38 |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\ddagger$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 30.00 |  |  | 25.00 |  |  | 25.00 |  |  | 30.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

## Volumes

| Name | W Railroad Ave |  |  | W Rairoad Ave |  |  | OR 38 |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 5 | 4 | 2 | 0 | 1 | 5 | 5 | 305 | 5 | 6 | 339 | 4 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 7.00 | 0.00 | 0.00 | 9.00 | 0.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 5 | 4 | 2 | 0 | 1 | 5 | 5 | 305 | 5 | 6 | 339 | 4 |
| Peak Hour Factor | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 1 | 1 | 1 | 0 | 0 | 1 | 1 | 83 | 1 | 2 | 92 | 1 |
| Total Analysis Volume [veh/h] | 5 | 4 | 2 | 0 | 1 | 5 | 5 | 332 | 5 | 7 | 368 | 4 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

Intersection Settings

| Priority Scheme | Stop | Stop | Free |  |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 16.09 | 15.66 | 10.35 | 15.89 | 15.44 | 10.36 | 8.02 | 0.00 | 0.00 | 7.94 | 0.00 | 0.00 |
| Movement LOS | C | C | B | C | C | B | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.09 | 0.09 | 0.09 | 0.03 | 0.03 | 0.03 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 |
| 95th-Percentile Queue Length [ft/ln] | 2.26 | 2.26 | 2.26 | 0.78 | 0.78 | 0.78 | 0.31 | 0.31 | 0.31 | 0.43 | 0.43 | 0.43 |
| d_A, Approach Delay [s/veh] |  | 14.89 |  |  | 11.20 |  |  | 0.12 |  |  | 0.15 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |
| d_I, Intersection Delay [s/veh] | 0.44 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |  |  |  |  |  |  |

## Generated with PTV VISTRO

27003 Reedsport Rail Crossing Study
HCM 6th Edition
Version 2022 (SP 0-2)
Year 2045 Traffic Conditions
Weekday PM Peak Hour

## Intersection Level Of Service Report

 Intersection 3: OR 38 / E Railroad AveControl Type: Analysis Method: Analysis Period:

Two-way stop
HCM 6 th Edition
15 minutes

| Delay (sec / veh): | 15.9 |
| :---: | :---: |
| Level Of Service: | C |
| Volume to Capacity $(\mathrm{v} / \mathrm{c}):$ | 0.006 |

C
0.006

Intersection Setup

| Name | E Railroad Ave |  |  | E Railroad Ave |  |  | OR 38 |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 30.00 |  |  | 25.00 |  |  | 25.00 |  |  | 30.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

## Volumes

| Name | E Rairoad Ave |  |  | E Rairoad Ave |  |  | OR 38 |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 0 | 4 | 4 | 0 | 2 | 21 | 25 | 278 | 6 | 1 | 330 | 1 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.00 | 0.00 | 0.00 | 8.00 | 0.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 0 | 4 | 4 | 0 | 2 | 21 | 25 | 278 | 6 | 1 | 330 | 1 |
| Peak Hour Factor | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 0 | 1 | 1 | 0 | 1 | 6 | 7 | 77 | 2 | 0 | 92 | 0 |
| Total Analysis Volume [veh/h] | 0 | 4 | 4 | 0 | 2 | 23 | 28 | 309 | 7 | 1 | 367 | 1 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

Intersection Settings

| Priority Scheme | Stop | Stop | Free |  |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.00 | 0.01 | 0.01 | 0.00 | 0.01 | 0.03 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 16.74 | 15.80 | 10.05 | 16.42 | 15.94 | 10.51 | 8.07 | 0.00 | 0.00 | 7.87 | 0.00 | 0.00 |
| Movement LOS | C | C | B | C | C | B | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.05 | 0.05 | 0.05 | 0.12 | 0.12 | 0.12 | 0.07 | 0.07 | 0.07 | 0.00 | 0.00 | 0.00 |
| 95th-Percentile Queue Length [ft/ln] | 1.32 | 1.32 | 1.32 | 3.09 | 3.09 | 3.09 | 1.79 | 1.79 | 1.79 | 0.06 | 0.06 | 0.06 |
| d_A, Approach Delay [s/veh] |  | 12.93 |  |  | 10.95 |  |  | 0.66 |  |  | 0.02 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |
| d_I, Intersection Delay [s/veh] | 0.82 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |  |  |  |  |  |  |

## Intersection Level Of Service Report Intersection 4: OR 38 / N 6th St

Control Type: Analysis Method: Analysis Period:

Two-way stop HCM 6th Edition 15 minutes

| Delay (sec / veh): | 15.4 |
| :---: | :---: |
| Level Of Service: | C |
| Volume to Capacity $(\mathrm{v} / \mathrm{c}):$ | 0.041 |

Intersection Setup

| Name | S 6th St |  | OR 38 |  | OR 38 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $T$ |  | $\stackrel{F}{x}$ |  | $4$ |  |
| Turning Movement | Left | Right | Thru | Right | Left | Thru |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 20.00 |  | 25.00 |  | 25.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

## Volumes

| Name | S 6 th St |  | OR 38 |  | OR 38 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 14 | 10 | 353 | 16 | 11 | 331 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 0.00 | 0.00 | 8.00 | 38.00 | 0.00 | 7.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 14 | 10 | 353 | 16 | 11 | 331 |
| Peak Hour Factor | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 | 0.9200 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 4 | 3 | 96 | 4 | 3 | 90 |
| Total Analysis Volume [veh/h] | 15 | 11 | 384 | 17 | 12 | 360 |
| Pedestrian Volume [ped/h] |  | 0 |  | 0 |  | 0 |

Version 2022 (SP 0-2)
Intersection Settings

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.04 | 0.02 | 0.00 | 0.00 | 0.01 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 15.39 | 10.94 | 0.00 | 0.00 | 8.11 | 0.00 |
| Movement LOS | C | B | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.18 | 0.18 | 0.00 | 0.00 | 0.03 | 0.03 |
| 95th-Percentile Queue Length [ft/ln] | 4.59 | 4.59 | 0.00 | 0.00 | 0.78 | 0.78 |
| d_A, Approach Delay [s/veh] | 13.51 |  | 0.00 |  | 0.26 |  |
| Approach LOS | B |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 0.56 |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |

## Intersection Level Of Service Report

## Intersection 5: OR 38 / Riverfront Way / Winchester

Control Type: Analysis Method: Analysis Period:

Two-way stop
HCM 6th Edition 15 minutes

Delay (sec / veh):
Level Of Service:
Volume to Capacity (v/c):
19.5

C
0.144

Intersection Setup

| Name | Winchester Ave |  |  | Riverfront Way |  |  | OR 38 |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\dagger$ |  |  | $\uparrow$ |  |  | $H$ |  |  | $7 F$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 50.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 450.00 | 250.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

Volumes

| Name | Winchester Ave |  |  | Riverfront Way |  |  | OR 38 |  |  | OR 38 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 34 | 7 | 1 | 4 | 2 | 18 | 6 | 263 | 6 | 31 | 256 | 7 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.00 | 20.00 | 4.00 | 12.00 | 0.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 34 | 7 | 1 | 4 | 2 | 18 | 6 | 263 | 6 | 31 | 256 | 7 |
| Peak Hour Factor | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 | 0.7900 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 11 | 2 | 0 | 1 | 1 | 6 | 2 | 83 | 2 | 10 | 81 | 2 |
| Total Analysis Volume [veh/h] | 43 | 9 | 1 | 5 | 3 | 23 | 8 | 333 | 8 | 39 | 324 | 9 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

Intersection Settings

| Priority Scheme | Stop | Stop | Free |  |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane |  | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.14 | 0.03 | 0.00 | 0.02 | 0.01 | 0.03 | 0.01 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 19.49 | 18.54 | 10.05 | 17.18 | 16.56 | 10.43 | 7.93 | 0.00 | 0.00 | 8.08 | 0.00 | 0.00 |
| Movement LOS | C | C | B | C | C | B | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.61 | 0.61 | 0.00 | 0.18 | 0.18 | 0.18 | 0.02 | 0.02 | 0.00 | 0.10 | 0.00 | 0.00 |
| 95th-Percentile Queue Length [ft/ln] | 15.24 | 15.24 | 0.11 | 4.58 | 4.58 | 4.58 | 0.49 | 0.49 | 0.00 | 2.50 | 0.00 | 0.00 |
| d_A, Approach Delay [s/veh] |  | 19.15 |  |  | 12.11 |  |  | 0.18 |  |  | 0.85 |  |
| Approach LOS |  | C |  |  | B |  |  | A |  |  | A |  |
| d_I, Intersection Delay [s/veh] | 2.20 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |  |  |  |  |  |  |

Control Type: Analysis Method: Analysis Period:

Signalized
HCM 6th Edition 15 minutes

Delay (sec / veh):
Level Of Service:
Volume to Capacity (v/c):
11.0

B
0.546

Intersection Setup

| Name | US 101 |  |  | US 101 |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $7 \\|$ |  |  | $7 \$$ |  |  | $H \Gamma$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 125.00 | 100.00 | 100.00 | 75.00 | 100.00 | 100.00 | 100.00 | 100.00 | 75.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 30.00 |  |  | 30.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Curb Present | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

Volumes

| Name | US 101 |  |  | US 101 |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 58 | 601 | 98 | 16 | 670 | 28 | 30 | 6 | 69 | 96 | 20 | 18 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 6.00 | 2.00 | 8.00 | 7.00 | 4.00 | 8.00 | 0.00 | 2.00 | 1.00 | 0.00 | 13.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Right Turn on Red Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 58 | 601 | 98 | 16 | 670 | 28 | 30 | 6 | 69 | 96 | 20 | 18 |
| Peak Hour Factor | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 | 0.9300 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 16 | 162 | 26 | 4 | 180 | 8 | 8 | 2 | 19 | 26 | 5 | 5 |
| Total Analysis Volume [veh/h] | 62 | 646 | 105 | 17 | 720 | 30 | 32 | 6 | 74 | 103 | 22 | 19 |
| Presence of On-Street Parking | No |  | No | No |  | No | No |  | No | No |  | No |
| On-Street Parking Maneuver Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Local Bus Stopping Rate [/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| v_do, Outbound Pedestrian Volume crossing | 2 |  |  | 1 |  |  | 0 |  |  | 1 |  |  |
| v_di, Inbound Pedestrian Volume crossing m | 0 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| v_co, Outbound Pedestrian Volume crossing | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| v_ci, Inbound Pedestrian Volume crossing rii | i 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| v_ab, Corner Pedestrian Volume [ped/h] | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Bicycle Volume [bicycles/h] | 0 |  |  | 7 |  |  | 0 |  |  | 0 |  |  |

27003 Reedsport Rail Crossing Study
HCM 6th Edition
Version 2022 (SP 0-2)
Year 2045 Traffic Conditions
Weekday PM Peak Hour
Intersection Settings

| Located in CBD |  |
| :---: | :---: |
| Signal Coordination Group |  |
| Cycle Length [s] |  |
| Coordination Type |  |
| Actuation Type | Free Running |
| Offset [s] | Fully actuated |
| Offset Reference | 0.0 |
| Permissive Mode | Lead Green - Beginning of First Green |
| Lost time [s] | SingleBand |
| 12.00 |  |

Phasing \& Timing

| Control Type | ProtPer | Permiss | Permiss | ProtPer | Permiss | Permiss | Permiss | Permiss | Permiss | Permiss | Permiss | Permiss |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal Group | 5 | 2 | 0 | 1 | 6 | 0 | 0 | 8 | 0 | 0 | 4 | 0 |
| Auxiliary Signal Groups |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead / Lag | Lead | - | - | Lead | - | - | - | - | - | - | - | - |
| Minimum Green [s] | 5 | 10 | 0 | 3 | 10 | 0 | 0 | 5 | 0 | 0 | 5 | 0 |
| Maximum Green [s] | 20 | 45 | 0 | 20 | 45 | 0 | 0 | 30 | 0 | 0 | 30 | 0 |
| Amber [s] | 3.5 | 3.8 | 0.0 | 3.5 | 3.8 | 0.0 | 0.0 | 3.5 | 0.0 | 0.0 | 3.5 | 0.0 |
| All red [s] | 1.6 | 1.3 | 0.0 | 1.6 | 1.6 | 0.0 | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 |
| Split [s] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Vehicle Extension [s] | 3.0 | 3.0 | 0.0 | 2.5 | 4.5 | 0.0 | 0.0 | 2.5 | 0.0 | 0.0 | 3.0 | 0.0 |
| Walk [s] | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 7 | 0 |
| Pedestrian Clearance [s] | 0 | 15 | 0 | 0 | 16 | 0 | 0 | 18 | 0 | 0 | 19 | 0 |
| Delayed Vehicle Green [s] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Rest In Walk |  | No |  |  | No |  |  | No |  |  | No |  |
| 11, Start-Up Lost Time [s] | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 |
| I2, Clearance Lost Time [s] | 3.1 | 3.1 | 0.0 | 3.1 | 3.4 | 0.0 | 0.0 | 3.5 | 0.0 | 0.0 | 3.5 | 0.0 |
| Minimum Recall | No | No |  | No | No |  |  | No |  |  | No |  |
| Maximum Recall | No | No |  | No | No |  |  | No |  |  | No |  |
| Pedestrian Recall | No | No |  | No | No |  |  | No |  |  | No |  |
| Detector Location [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector Length [ft] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| I, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

## Exclusive Pedestrian Phase

| Pedestrian Signal Group |  |
| :---: | :--- |
| Pedestrian Walk [s] |  |
| Pedestrian Clearance [s] |  |

## Lane Group Calculations

| Lane Group | L | C | C | L | C | C | C | R | C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C, Cycle Length [s] | 38 | 38 | 38 | 38 | 38 | 38 | 38 | 38 | 38 |
| L, Total Lost Time per Cycle [s] | 5.10 | 5.10 | 5.10 | 5.40 | 5.40 | 5.40 | 5.50 | 5.50 | 5.50 |
| 11_p, Permitted Start-Up Lost Time [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.00 | 0.00 | 2.00 |
| I2, Clearance Lost Time [s] | 0.00 | 3.10 | 3.10 | 0.00 | 3.40 | 3.40 | 3.50 | 3.50 | 3.50 |
| g_i, Effective Green Time [s] | 21 | 15 | 15 | 21 | 13 | 13 | 7 | 7 | 7 |
| $\mathrm{g} / \mathrm{C}, \mathrm{Green}$ / Cycle | 0.55 | 0.40 | 0.40 | 0.54 | 0.35 | 0.35 | 0.17 | 0.17 | 0.17 |
| (v / s)_i Volume / Saturation Flow Rate | 0.03 | 0.21 | 0.21 | 0.02 | 0.21 | 0.21 | 0.02 | 0.05 | 0.14 |
| s , saturation flow rate [veh/h] | 1781 | 1810 | 1723 | 854 | 1795 | 1765 | 1613 | 1584 | 996 |
| c, Capacity [veh/h] | 975 | 736 | 700 | 642 | 624 | 614 | 445 | 267 | 329 |
| d1, Uniform Delay [s] | 4.50 | 8.53 | 8.54 | 4.41 | 10.28 | 10.29 | 13.48 | 13.84 | 16.14 |
| k , delay calibration | 0.11 | 0.11 | 0.11 | 0.08 | 0.19 | 0.19 | 0.08 | 0.08 | 0.11 |
| I, Upstream Filtering Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| d2, Incremental Delay [s] | 0.03 | 0.58 | 0.61 | 0.01 | 1.62 | 1.66 | 0.06 | 0.42 | 0.91 |
| d3, Initial Queue Delay [s] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Rp, platoon ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| PF, progression factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

Lane Group Results

| X, volume / capacity | 0.06 | 0.52 | 0.52 | 0.03 | 0.60 | 0.61 | 0.09 | 0.28 | 0.44 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d, Delay for Lane Group [s/veh] | 4.53 | 9.11 | 9.14 | 4.42 | 11.90 | 11.95 | 13.54 | 14.26 |  |
| Lane Group LOS | A | A | A | A | B | B | B | B |  |
| Critical Lane Group | Yes | No | No | No | No | Yes | No | No | B |
| Yes |  |  |  |  |  |  |  |  |  |
| 50th-Percentile Queue Length [veh/ln] | 0.13 | 1.79 | 1.71 | 0.04 | 2.22 | 2.19 | 0.25 | 0.51 |  |
| 95th-Percentile Queue Length [veh/ln] | 0.23 | 3.23 | 3.09 | 0.06 | 3.99 | 3.95 | 0.44 | 0.15 |  |
| 95th-Percentile Queue Length [ft/ln] | 5.73 | 80.63 | 77.14 | 1.61 | 99.72 | 98.73 | 11.05 | 22.81 |  |

Movement, Approach, \& Intersection Results

| d_M, Delay for Movement [s/veh] | 4.53 | 9.12 | 9.14 | 4.42 | 11.92 | 11.95 | 13.54 | 13.54 | 14.26 | 17.05 | 17.05 | 17.05 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement LOS | A | A | A | A | B | B | B | B | B | B | B | B |
| d_A, Approach Delay [s/veh] | 8.78 |  |  | 11.76 |  |  | 14.01 |  |  | 17.05 |  |  |
| Approach LOS | A |  |  | B |  |  | B |  |  | B |  |  |
| d_l, Intersection Delay [s/veh] | 10.99 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Intersection V/C | 0.546 |  |  |  |  |  |  |  |  |  |  |  |

## Other Modes

| g_Walk,mi, Effective Walk Time [s] | 11.0 | 11.0 | 11.0 | 11.0 |
| :---: | :---: | :---: | :---: | :---: |
| M_corner, Corner Circulation Area [ft²/ped] | 0.00 | 0.00 | 0.00 | 0.00 |
| M_CW, Crosswalk Circulation Area [ft²/ped | 0.00 | 0.00 | 0.00 | 0.00 |
| d_p, Pedestrian Delay [s] | 9.67 | 9.67 | 9.67 | 9.67 |
| I_p,int, Pedestrian LOS Score for Intersectign | 2.728 | 2.685 | 1.990 | A |
| Crosswalk LOS | B | B | A |  |
| s_b, Saturation Flow Rate of the bicycle lan_ | 2000 | 2000 | 2000 | 2000 |
| c_b, Capacity of the bicycle lane [bicycles/h] | 2358 | 2358 | 1572 | 1572 |
| d_b, Bicycle Delay [s] | 0.61 | 0.61 | 0.87 | 0.87 |
| I_b,int, Bicycle LOS Score for Intersection | 2.230 | 2.192 | 1.744 | 1.797 |
| Bicycle LOS | B | B | A |  |

## Sequence

| Ring 1 | 1 | 2 | - | 4 | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ring 2 | 5 | 6 | - | 8 | - | - | - | - | - | - | - | - | - | - | - | - |
| Ring 3 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Ring 4 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |



## Intersection Level Of Service Report

Intersection 7: Winchester Ave / W Railroad Ave
Control Type:
Analysis Method:
Analysis Period:

> Two-way stop
> HCM 6th Edition
> 15 minutes
10.8
Delay (sec / veh):
Level Of Service:
Volume to Capacity ( $\mathrm{v} / \mathrm{c}$ ):

Intersection Setup

| Name | River Bend Rd |  |  | W Railroad Ave |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

## Volumes

| Name | River Bend Rd |  |  | W Raiload Ave |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 15 | 0 | 5 | 2 | 1 | 5 | 1 | 113 | 26 | 4 | 102 | 0 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 15 | 0 | 5 | 2 | 1 | 5 | 1 | 113 | 26 | 4 | 102 | 0 |
| Peak Hour Factor | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 | 0.8700 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 4 | 0 | 1 | 1 | 0 | 1 | 0 | 32 | 7 | 1 | 29 | 0 |
| Total Analysis Volume [veh/h] | 17 | 0 | 6 | 2 | 1 | 6 | 1 | 130 | 30 | 5 | 117 | 0 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

Intersection Settings

| Priority Scheme | Stop | Stop | Free |  |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.03 | 0.00 | 0.01 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 10.53 | 10.85 | 9.13 | 10.40 | 10.84 | 8.88 | 7.43 | 0.00 | 0.00 | 7.52 | 0.00 | 0.00 |
| Movement LOS | B | B | A | B | B | A | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.10 | 0.10 | 0.10 | 0.03 | 0.03 | 0.03 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 |
| 95th-Percentile Queue Length [ft/ln] | 2.47 | 2.47 | 2.47 | 0.83 | 0.83 | 0.83 | 0.05 | 0.05 | 0.05 | 0.26 | 0.26 | 0.26 |
| d_A, Approach Delay [s/veh] |  | 10.16 |  |  | 9.43 |  |  | 0.05 |  |  | 0.31 |  |
| Approach LOS |  | B |  |  | A |  |  | A |  |  | A |  |
| d_I, Intersection Delay [s/veh] | 1.15 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |

Control Type: Analysis Method: Analysis Period:

Two-way stop
HCM 6 th Edition
15 minutes

Delay (sec / veh):
Level Of Service:
Volume to Capacity ( $\mathrm{v} / \mathrm{c}$ ):
10.2

B
0.017

Intersection Setup

| Name | Elm Ave |  | Winchester Ave |  | Winchester Ave |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $T$ |  | $\stackrel{F}{x}$ |  | $4$ |  |
| Turning Movement | Left | Right | Thru | Right | Left | Thru |
| Lane Width [ft] | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  | 25.00 |  | 25.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

## Volumes

| Name | Elm Ave |  | Winchester Ave |  | Winchester Ave |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 11 | 5 | 122 | 6 | 2 | 124 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 0.00 | 0.00 | 3.00 | 0.00 | 0.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 11 | 5 | 122 | 6 | 2 | 124 |
| Peak Hour Factor | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 | 0.9000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 3 | 1 | 34 | 2 | 1 | 34 |
| Total Analysis Volume [veh/h] | 12 | 6 | 136 | 7 | 2 | 138 |
| Pedestrian Volume [ped/h] |  | 0 |  | 0 |  | 0 |

Version 2022 (SP 0-2)
Intersection Settings

| Priority Scheme | Stop | Free | Free |
| :---: | :---: | :---: | :---: |
| Flared Lane | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |
| Two-Stage Gap Acceptance | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 10.17 | 9.05 | 0.00 | 0.00 | 7.48 | 0.00 |
| Movement LOS | B | A | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.07 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 |
| 95th-Percentile Queue Length [ft/ln] | 1.80 | 1.80 | 0.00 | 0.00 | 0.10 | 0.10 |
| d_A, Approach Delay [s/veh] | 9.80 |  | 0.00 |  | 0.11 |  |
| Approach LOS | A |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 0.64 |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |

## Intersection Level Of Service Report

Intersection 9: Winchester Ave / E Railroad Ave

| Control Type: | Two-way stop | Delay $(\mathrm{sec} / \mathrm{veh}):$ | 10.9 |
| :---: | :---: | :---: | :---: |
| Analysis Method: | HCM 6th Edition | Level Of Service: | B |
| Analysis Period: | 15 minutes | Volume to Capacity $(\mathrm{v} / \mathrm{c}):$ | 0.018 |

Intersection Setup

| Name | Private Dwy |  |  | E Railroad Ave |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\ddagger$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Left | Right | Right2 | Left2 | Left | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 30.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

## Volumes

| Name | Private Dwy |  |  | E Rairoad Ave |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 10 | 4 | 0 | 1 | 1 | 27 | 17 | 106 | 6 | 2 | 97 | 2 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 0.00 | 0.00 | 2.00 | 0.00 | 0.00 | 0.00 | 7.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 10 | 4 | 0 | 1 | 1 | 27 | 17 | 106 | 6 | 2 | 97 | 2 |
| Peak Hour Factor | 0.8800 | 0.8800 | 1.0000 | 0.8800 | 0.8800 | 0.8800 | 0.8800 | 0.8800 | 0.8800 | 0.8800 | 0.8800 | 0.8800 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 3 | 1 | 0 | 0 | 0 | 8 | 5 | 30 | 2 | 1 | 28 | 1 |
| Total Analysis Volume [veh/h] | 11 | 5 | 0 | 1 | 1 | 31 | 19 | 120 | 7 | 2 | 110 | 2 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

Intersection Settings

| Priority Scheme | Stop | Stop | Free |  |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 | 0.03 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 10.95 | 9.04 | 9.01 | 10.53 | 10.52 | 8.94 | 7.52 | 0.00 | 0.00 | 7.45 | 0.00 | 0.00 |
| Movement LOS | B | A | A | B | B | A | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.07 | 0.07 | 0.07 | 0.11 | 0.11 | 0.11 | 0.04 | 0.04 | 0.04 | 0.00 | 0.00 | 0.00 |
| 95th-Percentile Queue Length [ft/ln] | 1.78 | 1.78 | 1.78 | 2.77 | 2.77 | 2.77 | 1.00 | 1.00 | 1.00 | 0.10 | 0.10 | 0.10 |
| d_A, Approach Delay [s/veh] |  | 10.35 |  |  | 9.04 |  |  | 0.98 |  |  | 0.13 |  |
| Approach LOS |  | B |  |  | A |  |  | A |  |  | A |  |
| d_I, Intersection Delay [s/veh] | 2.01 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |

## Generated with PTV VISTRO

27003 Reedsport Rail Crossing Study
HCM 6th Edition
Version 2022 (SP 0-2)
Year 2045 Traffic Conditions
Weekday PM Peak Hour

## Intersection Level Of Service Report

Intersection 10: Winchester Ave / S 6th St

## Control Type: Analysis Method: Analysis Period:

Two-way stop HCM 6th Edition 15 minutes
Delay (sec / veh):
Level Of Service:
Volume to Capacity (v/c):
10.5
B
0.013

Intersection Setup

| Name | S 6th St |  |  | S 6th St |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 | 11.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 20.00 |  |  | 25.00 |  |  | 25.00 |  |  | 30.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | No |  |  | No |  |  | No |  |  | No |  |  |

## Volumes

| Name | S 6 th St |  |  | S 6 th St |  |  | Winchester Ave |  |  | Winchester Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 7 | 4 | 1 | 1 | 7 | 9 | 6 | 81 | 14 | 0 | 69 | 0 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 17.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.00 | 0.00 | 0.00 | 2.00 | 0.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 7 | 4 | 1 | 1 | 7 | 9 | 6 | 81 | 14 | 0 | 69 | 0 |
| Peak Hour Factor | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 | 0.7800 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 2 | 1 | 0 | 0 | 2 | 3 | 2 | 26 | 4 | 0 | 22 | 0 |
| Total Analysis Volume [veh/h] | 9 | 5 | 1 | 1 | 9 | 12 | 8 | 104 | 18 | 0 | 88 | 0 |
| Pedestrian Volume [ped/h] |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |

Intersection Settings

| Priority Scheme | Stop | Stop | Free |  |
| :---: | :---: | :---: | :---: | :---: |
| Flared Lane | No | No |  |  |
| Storage Area [veh] | 0 | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | No |  |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |  |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.01 | 0.01 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 10.42 | 10.40 | 8.92 | 10.04 | 10.47 | 8.81 | 7.38 | 0.00 | 0.00 | 7.44 | 0.00 | 0.00 |
| Movement LOS | B | B | A | B | B | A | A | A | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.07 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 | 0.02 | 0.02 | 0.02 | 0.00 | 0.00 | 0.00 |
| 95th-Percentile Queue Length [ft/ln] | 1.66 | 1.66 | 1.66 | 2.08 | 2.08 | 2.08 | 0.40 | 0.40 | 0.40 | 0.00 | 0.00 | 0.00 |
| d_A, Approach Delay [s/veh] |  | 10.32 |  |  | 9.55 |  |  | 0.45 |  |  | 0.00 |  |
| Approach LOS |  | B |  |  | A |  |  | A |  |  | A |  |
| d_I, Intersection Delay [s/veh] | 1.66 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |

# Attachment B: Future Train Event Queueing Calculations 

|  | Existing |  |  | Existing |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 127 |  |  | 134 |  |  |
|  |  |  |  |  |  |
| 200 |  |  |  |  |  |
| k | Cumulative |  | k |  | ulative |
| 0 | 1.5\% | 1.5\% | 0 | 1.1\% | 1.1\% |
| 1 | 6.1\% | 7.6\% | 1 | 5.1\% | 6.3\% |
| 2 | 13.0\% | 20.6\% | 2 | 11.5\% | 17.7\% |
| 3 | 18.3\% | 38.9\% | 3 | 17.1\% | 34.8\% |
| 4 | 19.4\% | 58.3\% | 4 | 19.0\% | 53.8\% |
| 5 | 16.4\% | 74.8\% | 5 | 17.0\% | 70.9\% |
| 6 | 11.6\% | 86.4\% | 6 | 12.7\% | 83.5\% |
| 7 | 7.0\% | 93.4\% | 7 | 8.1\% | 91.6\% |
| 8 | 3.7\% | 97.1\% | 8 | 4.5\% | 96.1\% |
| 9 | 1.7\% | 98.8\% | 9 | 2.2\% | 98.4\% |
| 10 | 0.7\% | 99.6\% | 10 | 1.0\% | 99.4\% |
| 11 | 0.3\% | 99.9\% | 11 | 0.4\% | 99.8\% |
| 12 | 0.1\% | 100.0\% | 12 | 0.2\% | 99.9\% |
| 13 | 0.0\% | 100.0\% | 13 | 0.1\% | 100.0\% |
| 14 | 0.0\% | 100.0\% | 14 | 0.0\% | 100.0\% |
| 15 | 0.0\% | 100.0\% | 15 | 0.0\% | 100.0\% |
| 16 | 0.0\% | 100.0\% | 16 | 0.0\% | 100.0\% |
| 17 | 0.0\% | 100.0\% | 17 | 0.0\% | 100.0\% |
| 18 | 0.0\% | 100.0\% | 18 | 0.0\% | 100.0\% |
| 19 | 0.0\% | 100.0\% | 19 | 0.0\% | 100.0\% |
| 20 | 0.0\% | 100.0\% | 20 | 0.0\% | 100.0\% |
| 21 | 0.0\% | 100.0\% | 21 | 0.0\% | 100.0\% |
| 22 | 0.0\% | 100.0\% | 22 | 0.0\% | 100.0\% |
| 23 | 0.0\% | 100.0\% | 23 | 0.0\% | 100.0\% |
| 24 | 0.0\% | 100.0\% | 24 | 0.0\% | 100.0\% |
| 25 | 0.0\% | 100.0\% | 25 | 0.0\% | 100.0\% |
| 26 | 0.0\% | 100.0\% | 26 | 0.0\% | 100.0\% |
| 27 | 0.0\% | 100.0\% | 27 | 0.0\% | 100.0\% |
| 28 | 0.0\% | 100.0\% | 28 | 0.0\% | 100.0\% |
| 29 | 0.0\% | 100.0\% | 29 | 0.0\% | 100.0\% |
| 30 | 0.0\% | 100.0\% | 30 | 0.0\% | 100.0\% |
| 31 | 0.0\% | 100.0\% | 31 | 0.0\% | 100.0\% |
| 32 | 0.0\% | 100.0\% | 32 | 0.0\% | 100.0\% |
| 33 | 0.0\% | 100.0\% | 33 | 0.0\% | 100.0\% |
| 34 | 0.0\% | 100.0\% | 34 | 0.0\% | 100.0\% |
| 35 | 0.0\% | 100.0\% | 35 | 0.0\% | 100.0\% |
| 36 | 0.0\% | 100.0\% | 36 | 0.0\% | 100.0\% |
| 37 | 0.0\% | 100.0\% | 37 | 0.0\% | 100.0\% |
| 38 | 0.0\% | 100.0\% | 38 | 0.0\% | 100.0\% |
| 39 | 0.0\% | 100.0\% | 39 | 0.0\% | 100.0\% |


| 40 | 0.0\% | 100.0\% | 40 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | 0.0\% | 100.0\% | 41 | 0.0\% | 100.0\% |
| 42 | 0.0\% | 100.0\% | 42 | 0.0\% | 100.0\% |
| 43 | 0.0\% | 100.0\% | 43 | 0.0\% | 100.0\% |
| 44 | 0.0\% | 100.0\% | 44 | 0.0\% | 100.0\% |
| 45 | 0.0\% | 100.0\% | 45 | 0.0\% | 100.0\% |
| 46 | 0.0\% | 100.0\% | 46 | 0.0\% | 100.0\% |
| 47 | 0.0\% | 100.0\% | 47 | 0.0\% | 100.0\% |
| 48 | 0.0\% | 100.0\% | 48 | 0.0\% | 100.0\% |
| 49 | 0.0\% | 100.0\% | 49 | 0.0\% | 100.0\% |
| 50 | 0.0\% | 100.0\% | 50 | 0.0\% | 100.0\% |
| 51 | 0.0\% | 100.0\% | 51 | 0.0\% | 100.0\% |
| 52 | 0.0\% | 100.0\% | 52 | 0.0\% | 100.0\% |
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| 130 | 0.0\% | 100.0\% | 130 | 0.0\% | 100.0\% |
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| 307 |  |  | 351 |  |  |
|  |  |  |  |  |  |
| 550 |  |  |  |  |  |
| k |  | lative | k |  | ulative |
| 0 | 0.0\% | 0.0\% | 0 | 0.0\% | 0.0\% |
| 1 | 0.0\% | 0.0\% | 1 | 0.0\% | 0.0\% |
| 2 | 0.0\% | 0.0\% | 2 | 0.0\% | 0.0\% |
| 3 | 0.0\% | 0.0\% | 3 | 0.0\% | 0.0\% |
| 4 | 0.0\% | 0.1\% | 4 | 0.0\% | 0.0\% |
| 5 | 0.2\% | 0.2\% | 5 | 0.0\% | 0.0\% |
| 6 | 0.4\% | 0.6\% | 6 | 0.1\% | 0.1\% |
| 7 | 0.9\% | 1.5\% | 7 | 0.2\% | 0.4\% |
| 8 | 1.6\% | 3.1\% | 8 | 0.5\% | 0.9\% |
| 9 | 2.8\% | 5.9\% | 9 | 1.0\% | 2.0\% |
| 10 | 4.3\% | 10.2\% | 10 | 1.8\% | 3.8\% |
| 11 | 6.0\% | 16.3\% | 11 | 2.9\% | 6.7\% |
| 12 | 7.7\% | 24.0\% | 12 | 4.3\% | 11.0\% |
| 13 | 9.1\% | 33.1\% | 13 | 5.7\% | 16.7\% |
| 14 | 10.0\% | 43.0\% | 14 | 7.2\% | 23.9\% |
| 15 | 10.2\% | 53.2\% | 15 | 8.4\% | 32.3\% |
| 16 | 9.8\% | 63.0\% | 16 | 9.2\% | 41.6\% |
| 17 | 8.8\% | 71.9\% | 17 | 9.5\% | 51.1\% |
| 18 | 7.5\% | 79.4\% | 18 | 9.3\% | 60.4\% |
| 19 | 6.1\% | 85.5\% | 19 | 8.6\% | 69.0\% |
| 20 | 4.7\% | 90.2\% | 20 | 7.5\% | 76.6\% |
| 21 | 3.4\% | 93.6\% | 21 | 6.3\% | 82.9\% |
| 22 | 2.4\% | 96.0\% | 22 | 5.0\% | 87.9\% |
| 23 | 1.6\% | 97.5\% | 23 | 3.8\% | 91.7\% |
| 24 | 1.0\% | 98.6\% | 24 | 2.8\% | 94.5\% |
| 25 | 0.6\% | 99.2\% | 25 | 2.0\% | 96.5\% |
| 26 | 0.4\% | 99.6\% | 26 | 1.3\% | 97.8\% |
| 27 | 0.2\% | 99.8\% | 27 | 0.9\% | 98.7\% |
| 28 | 0.1\% | 99.9\% | 28 | 0.5\% | 99.2\% |
| 29 | 0.1\% | 99.9\% | 29 | 0.3\% | 99.6\% |
| 30 | 0.0\% | 100.0\% | 30 | 0.2\% | 99.8\% |
| 31 | 0.0\% | 100.0\% | 31 | 0.1\% | 99.9\% |
| 32 | 0.0\% | 100.0\% | 32 | 0.1\% | 99.9\% |
| 33 | 0.0\% | 100.0\% | 33 | 0.0\% | 100.0\% |
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| 41 | 0.0\% | 100.0\% | 41 | 0.0\% | 100.0\% |
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| 99 | 0.0\% | 100.0\% | 99 | 0.0\% | 100.0\% |
| 100 | 0.0\% | 100.0\% | 100 | 0.0\% | 100.0\% |
| 101 | 0.0\% | 100.0\% | 101 | 0.0\% | 100.0\% |
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| 112 | 0.0\% | 100.0\% | 112 | 0.0\% | 100.0\% |
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| 135 | 0.0\% | 100.0\% | 135 | 0.0\% | 100.0\% |
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| 137 | 0.0\% | 100.0\% | 137 | 0.0\% | 100.0\% |
| 138 | 0.0\% | 100.0\% | 138 | 0.0\% | 100.0\% |
| 139 | 0.0\% | 100.0\% | 139 | 0.0\% | 100.0\% |
| 140 | 0.0\% | 100.0\% | 140 | 0.0\% | 100.0\% |
| 141 | 0.0\% | 100.0\% | 141 | 0.0\% | 100.0\% |
| 142 | 0.0\% | 100.0\% | 142 | 0.0\% | 100.0\% |
| 143 | 0.0\% | 100.0\% | 143 | 0.0\% | 100.0\% |
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| 146 | 0.0\% | 100.0\% | 146 | 0.0\% | 100.0\% |
| 147 | 0.0\% | 100.0\% | 147 | 0.0\% | 100.0\% |
| 148 | 0.0\% | 100.0\% | 148 | 0.0\% | 100.0\% |
| 149 | 0.0\% | 100.0\% | 149 | 0.0\% | 100.0\% |
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|  | Existing |  |  | Existing |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 307 |  |  | 351 |  |  |
|  |  |  |  |  |  |
| 400 |  |  |  |  |  |
| k | Cumulative |  | k | Cumulative |  |
| 0 | 0.0\% | 0.0\% | 0 | 0.0\% | 0.0\% |
| 1 | 0.0\% | 0.0\% | 1 | 0.0\% | 0.0\% |
| 2 | 0.2\% | 0.2\% | 2 | 0.1\% | 0.1\% |
| 3 | 0.6\% | 0.9\% | 3 | 0.2\% | 0.3\% |
| 4 | 1.6\% | 2.5\% | 4 | 0.6\% | 0.9\% |
| 5 | 3.4\% | 5.9\% | 5 | 1.5\% | 2.5\% |
| 6 | 5.7\% | 11.6\% | 6 | 3.0\% | 5.4\% |
| 7 | 8.4\% | 20.0\% | 7 | 4.9\% | 10.3\% |
| 8 | 10.7\% | 30.7\% | 8 | 7.2\% | 17.6\% |
| 9 | 12.2\% | 42.9\% | 9 | 9.4\% | 27.0\% |
| 10 | 12.5\% | 55.4\% | 10 | 11.0\% | 37.9\% |
| 11 | 11.6\% | 67.0\% | 11 | 11.7\% | 49.6\% |
| 12 | 9.9\% | 76.9\% | 12 | 11.4\% | 61.0\% |
| 13 | 7.8\% | 84.7\% | 13 | 10.3\% | 71.3\% |
| 14 | 5.7\% | 90.4\% | 14 | 8.6\% | 79.8\% |
| 15 | 3.9\% | 94.3\% | 15 | 6.7\% | 86.5\% |
| 16 | 2.5\% | 96.8\% | 16 | 4.9\% | 91.4\% |
| 17 | 1.5\% | 98.2\% | 17 | 3.4\% | 94.8\% |
| 18 | 0.9\% | 99.1\% | 18 | 2.2\% | 97.0\% |
| 19 | 0.5\% | 99.6\% | 19 | 1.3\% | 98.3\% |
| 20 | 0.2\% | 99.8\% | 20 | 0.8\% | 99.1\% |
| 21 | 0.1\% | 99.9\% | 21 | 0.4\% | 99.5\% |
| 22 | 0.1\% | 100.0\% | 22 | 0.2\% | 99.8\% |
| 23 | 0.0\% | 100.0\% | 23 | 0.1\% | 99.9\% |
| 24 | 0.0\% | 100.0\% | 24 | 0.1\% | 100.0\% |
| 25 | 0.0\% | 100.0\% | 25 | 0.0\% | 100.0\% |
| 26 | 0.0\% | 100.0\% | 26 | 0.0\% | 100.0\% |
| 27 | 0.0\% | 100.0\% | 27 | 0.0\% | 100.0\% |
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| 30 | 0.0\% | 100.0\% | 30 | 0.0\% | 100.0\% |
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| 38 | 0.0\% | 100.0\% | 38 | 0.0\% | 100.0\% |
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| 40 | 0.0\% | 100.0\% | 40 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | 0.0\% | 100.0\% | 41 | 0.0\% | 100.0\% |
| 42 | 0.0\% | 100.0\% | 42 | 0.0\% | 100.0\% |
| 43 | 0.0\% | 100.0\% | 43 | 0.0\% | 100.0\% |
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| 47 | 0.0\% | 100.0\% | 47 | 0.0\% | 100.0\% |
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| 87 | 0.0\% | 100.0\% | 87 | 0.0\% | 100.0\% |
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| 88 | 0.0\% | 100.0\% | 88 | 0.0\% | 100.0\% |
| 89 | 0.0\% | 100.0\% | 89 | 0.0\% | 100.0\% |
| 90 | 0.0\% | 100.0\% | 90 | 0.0\% | 100.0\% |
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| 92 | 0.0\% | 100.0\% | 92 | 0.0\% | 100.0\% |
| 93 | 0.0\% | 100.0\% | 93 | 0.0\% | 100.0\% |
| 94 | 0.0\% | 100.0\% | 94 | 0.0\% | 100.0\% |
| 95 | 0.0\% | 100.0\% | 95 | 0.0\% | 100.0\% |
| 96 | 0.0\% | 100.0\% | 96 | 0.0\% | 100.0\% |
| 97 | 0.0\% | 100.0\% | 97 | 0.0\% | 100.0\% |
| 98 | 0.0\% | 100.0\% | 98 | 0.0\% | 100.0\% |
| 99 | 0.0\% | 100.0\% | 99 | 0.0\% | 100.0\% |
| 100 | 0.0\% | 100.0\% | 100 | 0.0\% | 100.0\% |
| 101 | 0.0\% | 100.0\% | 101 | 0.0\% | 100.0\% |
| 102 | 0.0\% | 100.0\% | 102 | 0.0\% | 100.0\% |
| 103 | 0.0\% | 100.0\% | 103 | 0.0\% | 100.0\% |
| 104 | 0.0\% | 100.0\% | 104 | 0.0\% | 100.0\% |
| 105 | 0.0\% | 100.0\% | 105 | 0.0\% | 100.0\% |
| 106 | 0.0\% | 100.0\% | 106 | 0.0\% | 100.0\% |
| 107 | 0.0\% | 100.0\% | 107 | 0.0\% | 100.0\% |
| 108 | 0.0\% | 100.0\% | 108 | 0.0\% | 100.0\% |
| 109 | 0.0\% | 100.0\% | 109 | 0.0\% | 100.0\% |
| 110 | 0.0\% | 100.0\% | 110 | 0.0\% | 100.0\% |
| 111 | 0.0\% | 100.0\% | 111 | 0.0\% | 100.0\% |
| 112 | 0.0\% | 100.0\% | 112 | 0.0\% | 100.0\% |
| 113 | 0.0\% | 100.0\% | 113 | 0.0\% | 100.0\% |
| 114 | 0.0\% | 100.0\% | 114 | 0.0\% | 100.0\% |
| 115 | 0.0\% | 100.0\% | 115 | 0.0\% | 100.0\% |
| 116 | 0.0\% | 100.0\% | 116 | 0.0\% | 100.0\% |
| 117 | 0.0\% | 100.0\% | 117 | 0.0\% | 100.0\% |
| 118 | 0.0\% | 100.0\% | 118 | 0.0\% | 100.0\% |
| 119 | 0.0\% | 100.0\% | 119 | 0.0\% | 100.0\% |
| 120 | 0.0\% | 100.0\% | 120 | 0.0\% | 100.0\% |
| 121 | 0.0\% | 100.0\% | 121 | 0.0\% | 100.0\% |
| 122 | 0.0\% | 100.0\% | 122 | 0.0\% | 100.0\% |
| 123 | 0.0\% | 100.0\% | 123 | 0.0\% | 100.0\% |
| 124 | 0.0\% | 100.0\% | 124 | 0.0\% | 100.0\% |
| 125 | 0.0\% | 100.0\% | 125 | 0.0\% | 100.0\% |
| 126 | 0.0\% | 100.0\% | 126 | 0.0\% | 100.0\% |
| 127 | 0.0\% | 100.0\% | 127 | 0.0\% | 100.0\% |
| 128 | 0.0\% | 100.0\% | 128 | 0.0\% | 100.0\% |
| 129 | 0.0\% | 100.0\% | 129 | 0.0\% | 100.0\% |
| 130 | 0.0\% | 100.0\% | 130 | 0.0\% | 100.0\% |
| 131 | 0.0\% | 100.0\% | 131 | 0.0\% | 100.0\% |
| 132 | 0.0\% | 100.0\% | 132 | 0.0\% | 100.0\% |
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| 134 | 0.0\% | 100.0\% | 134 | 0.0\% | 100.0\% |
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| 135 | 0.0\% | 100.0\% | 135 | 0.0\% | 100.0\% |
| 136 | 0.0\% | 100.0\% | 136 | 0.0\% | 100.0\% |
| 137 | 0.0\% | 100.0\% | 137 | 0.0\% | 100.0\% |
| 138 | 0.0\% | 100.0\% | 138 | 0.0\% | 100.0\% |
| 139 | 0.0\% | 100.0\% | 139 | 0.0\% | 100.0\% |
| 140 | 0.0\% | 100.0\% | 140 | 0.0\% | 100.0\% |
| 141 | 0.0\% | 100.0\% | 141 | 0.0\% | 100.0\% |
| 142 | 0.0\% | 100.0\% | 142 | 0.0\% | 100.0\% |
| 143 | 0.0\% | 100.0\% | 143 | 0.0\% | 100.0\% |
| 144 | 0.0\% | 100.0\% | 144 | 0.0\% | 100.0\% |
| 145 | 0.0\% | 100.0\% | 145 | 0.0\% | 100.0\% |
| 146 | 0.0\% | 100.0\% | 146 | 0.0\% | 100.0\% |
| 147 | 0.0\% | 100.0\% | 147 | 0.0\% | 100.0\% |
| 148 | 0.0\% | 100.0\% | 148 | 0.0\% | 100.0\% |
| 149 | 0.0\% | 100.0\% | 149 | 0.0\% | 100.0\% |
| 150 | 0.0\% | 100.0\% | 150 | 0.0\% | 100.0\% |


| PM | 2045 @ 10 mph |  | PM | 2045 @ 10 mph |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 5 |  |  |
| 307 |  |  | 351 |  |  |
|  |  |  |  |  |  |
| 850 |  |  | 950 |  |  |
| k |  | tive | k |  | ative |
| 0 | 0.0\% | 0.0\% | 0 | 0.0\% | 0.0\% |
| 1 | 0.0\% | 0.0\% | 1 | 0.0\% | 0.0\% |
| 2 | 0.0\% | 0.0\% | 2 | 0.0\% | 0.0\% |
| 3 | 0.0\% | 0.0\% | 3 | 0.0\% | 0.0\% |
| 4 | 0.0\% | 0.0\% | 4 | 0.0\% | 0.0\% |
| 5 | 0.0\% | 0.0\% | 5 | 0.0\% | 0.0\% |
| 6 | 0.0\% | 0.0\% | 6 | 0.0\% | 0.0\% |
| 7 | 0.0\% | 0.0\% | 7 | 0.0\% | 0.0\% |
| 8 | 0.0\% | 0.0\% | 8 | 0.0\% | 0.0\% |
| 9 | 0.0\% | 0.0\% | 9 | 0.0\% | 0.0\% |
| 10 | 0.0\% | 0.0\% | 10 | 0.0\% | 0.0\% |
| 11 | 0.1\% | 0.1\% | 11 | 0.0\% | 0.0\% |
| 12 | 0.1\% | 0.2\% | 12 | 0.0\% | 0.0\% |
| 13 | 0.3\% | 0.5\% | 13 | 0.0\% | 0.1\% |
| 14 | 0.5\% | 0.9\% | 14 | 0.1\% | 0.1\% |
| 15 | 0.8\% | 1.7\% | 15 | 0.1\% | 0.3\% |
| 16 | 1.2\% | 3.0\% | 16 | 0.3\% | 0.6\% |
| 17 | 1.9\% | 4.8\% | 17 | 0.5\% | 1.0\% |
| 18 | 2.7\% | 7.5\% | 18 | 0.8\% | 1.8\% |
| 19 | 3.6\% | 11.1\% | 19 | 1.2\% | 3.0\% |
| 20 | 4.6\% | 15.7\% | 20 | 1.7\% | 4.7\% |
| 21 | 5.6\% | 21.3\% | 21 | 2.4\% | 7.1\% |
| 22 | 6.5\% | 27.8\% | 22 | 3.2\% | 10.2\% |
| 23 | 7.2\% | 35.0\% | 23 | 4.0\% | 14.3\% |
| 24 | 7.7\% | 42.8\% | 24 | 4.9\% | 19.2\% |
| 25 | 7.9\% | 50.7\% | 25 | 5.7\% | 24.9\% |
| 26 | 7.8\% | 58.4\% | 26 | 6.5\% | 31.4\% |


| 27 | 7.4\% | 65.8\% | 27 | 7.0\% | 38.4\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 28 | 6.7\% | 72.5\% | 28 | 7.3\% | 45.7\% |
| 29 | 5.9\% | 78.5\% | 29 | 7.4\% | 53.1\% |
| 30 | 5.1\% | 83.5\% | 30 | 7.2\% | 60.3\% |
| 31 | 4.2\% | 87.7\% | 31 | 6.8\% | 67.1\% |
| 32 | 3.3\% | 91.0\% | 32 | 6.2\% | 73.3\% |
| 33 | 2.6\% | 93.6\% | 33 | 5.5\% | 78.8\% |
| 34 | 1.9\% | 95.6\% | 34 | 4.7\% | 83.5\% |
| 35 | 1.4\% | 97.0\% | 35 | 4.0\% | 87.4\% |
| 36 | 1.0\% | 98.0\% | 36 | 3.2\% | 90.7\% |
| 37 | 0.7\% | 98.7\% | 37 | 2.5\% | 93.2\% |
| 38 | 0.5\% | 99.2\% | 38 | 2.0\% | 95.2\% |
| 39 | 0.3\% | 99.5\% | 39 | 1.5\% | 96.6\% |
| 40 | 0.2\% | 99.7\% | 40 | 1.1\% | 97.7\% |
| 41 | 0.1\% | 99.8\% | 41 | 0.8\% | 98.5\% |
| 42 | 0.1\% | 99.9\% | 42 | 0.5\% | 99.0\% |
| 43 | 0.0\% | 99.9\% | 43 | 0.4\% | 99.4\% |
| 44 | 0.0\% | 100.0\% | 44 | 0.2\% | 99.6\% |
| 45 | 0.0\% | 100.0\% | 45 | 0.2\% | 99.7\% |
| 46 | 0.0\% | 100.0\% | 46 | 0.1\% | 99.8\% |
| 47 | 0.0\% | 100.0\% | 47 | 0.1\% | 99.9\% |
| 48 | 0.0\% | 100.0\% | 48 | 0.0\% | 99.9\% |
| 49 | 0.0\% | 100.0\% | 49 | 0.0\% | 100.0\% |
| 50 | 0.0\% | 100.0\% | 50 | 0.0\% | 100.0\% |
| 51 | 0.0\% | 100.0\% | 51 | 0.0\% | 100.0\% |
| 52 | 0.0\% | 100.0\% | 52 | 0.0\% | 100.0\% |
| 53 | 0.0\% | 100.0\% | 53 | 0.0\% | 100.0\% |
| 54 | 0.0\% | 100.0\% | 54 | 0.0\% | 100.0\% |
| 55 | 0.0\% | 100.0\% | 55 | 0.0\% | 100.0\% |
| 56 | 0.0\% | 100.0\% | 56 | 0.0\% | 100.0\% |
| 57 | 0.0\% | 100.0\% | 57 | 0.0\% | 100.0\% |
| 58 | 0.0\% | 100.0\% | 58 | 0.0\% | 100.0\% |
| 59 | 0.0\% | 100.0\% | 59 | 0.0\% | 100.0\% |
| 60 | 0.0\% | 100.0\% | 60 | 0.0\% | 100.0\% |


| 61 | 0.0\% | 100.0\% | 61 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 62 | 0.0\% | 100.0\% | 62 | 0.0\% | 100.0\% |
| 63 | 0.0\% | 100.0\% | 63 | 0.0\% | 100.0\% |
| 64 | 0.0\% | 100.0\% | 64 | 0.0\% | 100.0\% |
| 65 | 0.0\% | 100.0\% | 65 | 0.0\% | 100.0\% |
| 66 | 0.0\% | 100.0\% | 66 | 0.0\% | 100.0\% |
| 67 | 0.0\% | 100.0\% | 67 | 0.0\% | 100.0\% |
| 68 | 0.0\% | 100.0\% | 68 | 0.0\% | 100.0\% |
| 69 | 0.0\% | 100.0\% | 69 | 0.0\% | 100.0\% |
| 70 | 0.0\% | 100.0\% | 70 | 0.0\% | 100.0\% |
| 71 | 0.0\% | 100.0\% | 71 | 0.0\% | 100.0\% |
| 72 | 0.0\% | 100.0\% | 72 | 0.0\% | 100.0\% |
| 73 | 0.0\% | 100.0\% | 73 | 0.0\% | 100.0\% |
| 74 | 0.0\% | 100.0\% | 74 | 0.0\% | 100.0\% |
| 75 | 0.0\% | 100.0\% | 75 | 0.0\% | 100.0\% |
| 76 | 0.0\% | 100.0\% | 76 | 0.0\% | 100.0\% |
| 77 | 0.0\% | 100.0\% | 77 | 0.0\% | 100.0\% |
| 78 | 0.0\% | 100.0\% | 78 | 0.0\% | 100.0\% |
| 79 | 0.0\% | 100.0\% | 79 | 0.0\% | 100.0\% |
| 80 | 0.0\% | 100.0\% | 80 | 0.0\% | 100.0\% |
| 81 | 0.0\% | 100.0\% | 81 | 0.0\% | 100.0\% |
| 82 | 0.0\% | 100.0\% | 82 | 0.0\% | 100.0\% |
| 83 | 0.0\% | 100.0\% | 83 | 0.0\% | 100.0\% |
| 84 | 0.0\% | 100.0\% | 84 | 0.0\% | 100.0\% |
| 85 | 0.0\% | 100.0\% | 85 | 0.0\% | 100.0\% |
| 86 | 0.0\% | 100.0\% | 86 | 0.0\% | 100.0\% |
| 87 | 0.0\% | 100.0\% | 87 | 0.0\% | 100.0\% |
| 88 | 0.0\% | 100.0\% | 88 | 0.0\% | 100.0\% |
| 89 | 0.0\% | 100.0\% | 89 | 0.0\% | 100.0\% |
| 90 | 0.0\% | 100.0\% | 90 | 0.0\% | 100.0\% |
| 91 | 0.0\% | 100.0\% | 91 | 0.0\% | 100.0\% |
| 92 | 0.0\% | 100.0\% | 92 | 0.0\% | 100.0\% |
| 93 | 0.0\% | 100.0\% | 93 | 0.0\% | 100.0\% |
| 94 | 0.0\% | 100.0\% | 94 | 0.0\% | 100.0\% |


| 95 | 0.0\% | 100.0\% | 95 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 96 | 0.0\% | 100.0\% | 96 | 0.0\% | 100.0\% |
| 97 | 0.0\% | 100.0\% | 97 | 0.0\% | 100.0\% |
| 98 | 0.0\% | 100.0\% | 98 | 0.0\% | 100.0\% |
| 99 | 0.0\% | 100.0\% | 99 | 0.0\% | 100.0\% |
| 100 | 0.0\% | 100.0\% | 100 | 0.0\% | 100.0\% |
| 101 | 0.0\% | 100.0\% | 101 | 0.0\% | 100.0\% |
| 102 | 0.0\% | 100.0\% | 102 | 0.0\% | 100.0\% |
| 103 | 0.0\% | 100.0\% | 103 | 0.0\% | 100.0\% |
| 104 | 0.0\% | 100.0\% | 104 | 0.0\% | 100.0\% |
| 105 | 0.0\% | 100.0\% | 105 | 0.0\% | 100.0\% |
| 106 | 0.0\% | 100.0\% | 106 | 0.0\% | 100.0\% |
| 107 | 0.0\% | 100.0\% | 107 | 0.0\% | 100.0\% |
| 108 | 0.0\% | 100.0\% | 108 | 0.0\% | 100.0\% |
| 109 | 0.0\% | 100.0\% | 109 | 0.0\% | 100.0\% |
| 110 | 0.0\% | 100.0\% | 110 | 0.0\% | 100.0\% |
| 111 | 0.0\% | 100.0\% | 111 | 0.0\% | 100.0\% |
| 112 | 0.0\% | 100.0\% | 112 | 0.0\% | 100.0\% |
| 113 | 0.0\% | 100.0\% | 113 | 0.0\% | 100.0\% |
| 114 | 0.0\% | 100.0\% | 114 | 0.0\% | 100.0\% |
| 115 | 0.0\% | 100.0\% | 115 | 0.0\% | 100.0\% |
| 116 | 0.0\% | 100.0\% | 116 | 0.0\% | 100.0\% |
| 117 | 0.0\% | 100.0\% | 117 | 0.0\% | 100.0\% |
| 118 | 0.0\% | 100.0\% | 118 | 0.0\% | 100.0\% |
| 119 | 0.0\% | 100.0\% | 119 | 0.0\% | 100.0\% |
| 120 | 0.0\% | 100.0\% | 120 | 0.0\% | 100.0\% |
| 121 | 0.0\% | 100.0\% | 121 | 0.0\% | 100.0\% |
| 122 | 0.0\% | 100.0\% | 122 | 0.0\% | 100.0\% |
| 123 | 0.0\% | 100.0\% | 123 | 0.0\% | 100.0\% |
| 124 | 0.0\% | 100.0\% | 124 | 0.0\% | 100.0\% |
| 125 | 0.0\% | 100.0\% | 125 | 0.0\% | 100.0\% |
| 126 | 0.0\% | 100.0\% | 126 | 0.0\% | 100.0\% |
| 127 | 0.0\% | 100.0\% | 127 | 0.0\% | 100.0\% |
| 128 | 0.0\% | 100.0\% | 128 | 0.0\% | 100.0\% |


| 129 | 0.0\% | 100.0\% | 129 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 130 | 0.0\% | 100.0\% | 130 | 0.0\% | 100.0\% |
| 131 | 0.0\% | 100.0\% | 131 | 0.0\% | 100.0\% |
| 132 | 0.0\% | 100.0\% | 132 | 0.0\% | 100.0\% |
| 133 | 0.0\% | 100.0\% | 133 | 0.0\% | 100.0\% |
| 134 | 0.0\% | 100.0\% | 134 | 0.0\% | 100.0\% |
| 135 | 0.0\% | 100.0\% | 135 | 0.0\% | 100.0\% |
| 136 | 0.0\% | 100.0\% | 136 | 0.0\% | 100.0\% |
| 137 | 0.0\% | 100.0\% | 137 | 0.0\% | 100.0\% |
| 138 | 0.0\% | 100.0\% | 138 | 0.0\% | 100.0\% |
| 139 | 0.0\% | 100.0\% | 139 | 0.0\% | 100.0\% |
| 140 | 0.0\% | 100.0\% | 140 | 0.0\% | 100.0\% |
| 141 | 0.0\% | 100.0\% | 141 | 0.0\% | 100.0\% |
| 142 | 0.0\% | 100.0\% | 142 | 0.0\% | 100.0\% |
| 143 | 0.0\% | 100.0\% | 143 | 0.0\% | 100.0\% |
| 144 | 0.0\% | 100.0\% | 144 | 0.0\% | 100.0\% |
| 145 | 0.0\% | 100.0\% | 145 | 0.0\% | 100.0\% |
| 146 | 0.0\% | 100.0\% | 146 | 0.0\% | 100.0\% |
| 147 | 0.0\% | 100.0\% | 147 | 0.0\% | 100.0\% |
| 148 | 0.0\% | 100.0\% | 148 | 0.0\% | 100.0\% |
| 149 | 0.0\% | 100.0\% | 149 | 0.0\% | 100.0\% |
| 150 | 0.0\% | 100.0\% | 150 | 0.0\% | 100.0\% |

2045 OR38 - Non- Mixed Freight @ 10 mph with a 4300 ft train length


| 27 | 7.0\% | 38.3\% | 27 | 3.9\% | 15.1\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 28 | 7.3\% | 45.6\% | 28 | 4.7\% | 19.8\% |
| 29 | 7.4\% | 53.0\% | 29 | 5.4\% | 25.2\% |
| 30 | 7.2\% | 60.2\% | 30 | 6.0\% | 31.2\% |
| 31 | 6.8\% | 66.9\% | 31 | 6.5\% | 37.7\% |
| 32 | 6.2\% | 73.2\% | 32 | 6.8\% | 44.5\% |
| 33 | 5.5\% | 78.7\% | 33 | 6.9\% | 51.4\% |
| 34 | 4.7\% | 83.4\% | 34 | 6.8\% | 58.2\% |
| 35 | 4.0\% | 87.4\% | 35 | 6.5\% | 64.7\% |
| 36 | 3.2\% | 90.6\% | 36 | 6.0\% | 70.8\% |
| 37 | 2.6\% | 93.2\% | 37 | 5.5\% | 76.2\% |
| 38 | 2.0\% | 95.1\% | 38 | 4.8\% | 81.0\% |
| 39 | 1.5\% | 96.6\% | 39 | 4.1\% | 85.2\% |
| 40 | 1.1\% | 97.7\% | 40 | 3.5\% | 88.6\% |
| 41 | 0.8\% | 98.4\% | 41 | 2.8\% | 91.4\% |
| 42 | 0.5\% | 99.0\% | 42 | 2.2\% | 93.7\% |
| 43 | 0.4\% | 99.3\% | 43 | 1.7\% | 95.4\% |
| 44 | 0.2\% | 99.6\% | 44 | 1.3\% | 96.7\% |
| 45 | 0.2\% | 99.7\% | 45 | 1.0\% | 97.7\% |
| 46 | 0.1\% | 99.8\% | 46 | 0.7\% | 98.4\% |
| 47 | 0.1\% | 99.9\% | 47 | 0.5\% | 99.0\% |
| 48 | 0.0\% | 99.9\% | 48 | 0.4\% | 99.3\% |
| 49 | 0.0\% | 100.0\% | 49 | 0.2\% | 99.6\% |
| 50 | 0.0\% | 100.0\% | 50 | 0.2\% | 99.7\% |
| 51 | 0.0\% | 100.0\% | 51 | 0.1\% | 99.8\% |
| 52 | 0.0\% | 100.0\% | 52 | 0.1\% | 99.9\% |
| 53 | 0.0\% | 100.0\% | 53 | 0.0\% | 99.9\% |
| 54 | 0.0\% | 100.0\% | 54 | 0.0\% | 100.0\% |
| 55 | 0.0\% | 100.0\% | 55 | 0.0\% | 100.0\% |
| 56 | 0.0\% | 100.0\% | 56 | 0.0\% | 100.0\% |
| 57 | 0.0\% | 100.0\% | 57 | 0.0\% | 100.0\% |
| 58 | 0.0\% | 100.0\% | 58 | 0.0\% | 100.0\% |
| 59 | 0.0\% | 100.0\% | 59 | 0.0\% | 100.0\% |
| 60 | 0.0\% | 100.0\% | 60 | 0.0\% | 100.0\% |


| 61 | 0.0\% | 100.0\% | 61 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 62 | 0.0\% | 100.0\% | 62 | 0.0\% | 100.0\% |
| 63 | 0.0\% | 100.0\% | 63 | 0.0\% | 100.0\% |
| 64 | 0.0\% | 100.0\% | 64 | 0.0\% | 100.0\% |
| 65 | 0.0\% | 100.0\% | 65 | 0.0\% | 100.0\% |
| 66 | 0.0\% | 100.0\% | 66 | 0.0\% | 100.0\% |
| 67 | 0.0\% | 100.0\% | 67 | 0.0\% | 100.0\% |
| 68 | 0.0\% | 100.0\% | 68 | 0.0\% | 100.0\% |
| 69 | 0.0\% | 100.0\% | 69 | 0.0\% | 100.0\% |
| 70 | 0.0\% | 100.0\% | 70 | 0.0\% | 100.0\% |
| 71 | 0.0\% | 100.0\% | 71 | 0.0\% | 100.0\% |
| 72 | 0.0\% | 100.0\% | 72 | 0.0\% | 100.0\% |
| 73 | 0.0\% | 100.0\% | 73 | 0.0\% | 100.0\% |
| 74 | 0.0\% | 100.0\% | 74 | 0.0\% | 100.0\% |
| 75 | 0.0\% | 100.0\% | 75 | 0.0\% | 100.0\% |
| 76 | 0.0\% | 100.0\% | 76 | 0.0\% | 100.0\% |
| 77 | 0.0\% | 100.0\% | 77 | 0.0\% | 100.0\% |
| 78 | 0.0\% | 100.0\% | 78 | 0.0\% | 100.0\% |
| 79 | 0.0\% | 100.0\% | 79 | 0.0\% | 100.0\% |
| 80 | 0.0\% | 100.0\% | 80 | 0.0\% | 100.0\% |
| 81 | 0.0\% | 100.0\% | 81 | 0.0\% | 100.0\% |
| 82 | 0.0\% | 100.0\% | 82 | 0.0\% | 100.0\% |
| 83 | 0.0\% | 100.0\% | 83 | 0.0\% | 100.0\% |
| 84 | 0.0\% | 100.0\% | 84 | 0.0\% | 100.0\% |
| 85 | 0.0\% | 100.0\% | 85 | 0.0\% | 100.0\% |
| 86 | 0.0\% | 100.0\% | 86 | 0.0\% | 100.0\% |
| 87 | 0.0\% | 100.0\% | 87 | 0.0\% | 100.0\% |
| 88 | 0.0\% | 100.0\% | 88 | 0.0\% | 100.0\% |
| 89 | 0.0\% | 100.0\% | 89 | 0.0\% | 100.0\% |
| 90 | 0.0\% | 100.0\% | 90 | 0.0\% | 100.0\% |
| 91 | 0.0\% | 100.0\% | 91 | 0.0\% | 100.0\% |
| 92 | 0.0\% | 100.0\% | 92 | 0.0\% | 100.0\% |
| 93 | 0.0\% | 100.0\% | 93 | 0.0\% | 100.0\% |
| 94 | 0.0\% | 100.0\% | 94 | 0.0\% | 100.0\% |


| 95 | 0.0\% | 100.0\% | 95 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 96 | 0.0\% | 100.0\% | 96 | 0.0\% | 100.0\% |
| 97 | 0.0\% | 100.0\% | 97 | 0.0\% | 100.0\% |
| 98 | 0.0\% | 100.0\% | 98 | 0.0\% | 100.0\% |
| 99 | 0.0\% | 100.0\% | 99 | 0.0\% | 100.0\% |
| 100 | 0.0\% | 100.0\% | 100 | 0.0\% | 100.0\% |
| 101 | 0.0\% | 100.0\% | 101 | 0.0\% | 100.0\% |
| 102 | 0.0\% | 100.0\% | 102 | 0.0\% | 100.0\% |
| 103 | 0.0\% | 100.0\% | 103 | 0.0\% | 100.0\% |
| 104 | 0.0\% | 100.0\% | 104 | 0.0\% | 100.0\% |
| 105 | 0.0\% | 100.0\% | 105 | 0.0\% | 100.0\% |
| 106 | 0.0\% | 100.0\% | 106 | 0.0\% | 100.0\% |
| 107 | 0.0\% | 100.0\% | 107 | 0.0\% | 100.0\% |
| 108 | 0.0\% | 100.0\% | 108 | 0.0\% | 100.0\% |
| 109 | 0.0\% | 100.0\% | 109 | 0.0\% | 100.0\% |
| 110 | 0.0\% | 100.0\% | 110 | 0.0\% | 100.0\% |
| 111 | 0.0\% | 100.0\% | 111 | 0.0\% | 100.0\% |
| 112 | 0.0\% | 100.0\% | 112 | 0.0\% | 100.0\% |
| 113 | 0.0\% | 100.0\% | 113 | 0.0\% | 100.0\% |
| 114 | 0.0\% | 100.0\% | 114 | 0.0\% | 100.0\% |
| 115 | 0.0\% | 100.0\% | 115 | 0.0\% | 100.0\% |
| 116 | 0.0\% | 100.0\% | 116 | 0.0\% | 100.0\% |
| 117 | 0.0\% | 100.0\% | 117 | 0.0\% | 100.0\% |
| 118 | 0.0\% | 100.0\% | 118 | 0.0\% | 100.0\% |
| 119 | 0.0\% | 100.0\% | 119 | 0.0\% | 100.0\% |
| 120 | 0.0\% | 100.0\% | 120 | 0.0\% | 100.0\% |
| 121 | 0.0\% | 100.0\% | 121 | 0.0\% | 100.0\% |
| 122 | 0.0\% | 100.0\% | 122 | 0.0\% | 100.0\% |
| 123 | 0.0\% | 100.0\% | 123 | 0.0\% | 100.0\% |
| 124 | 0.0\% | 100.0\% | 124 | 0.0\% | 100.0\% |
| 125 | 0.0\% | 100.0\% | 125 | 0.0\% | 100.0\% |
| 126 | 0.0\% | 100.0\% | 126 | 0.0\% | 100.0\% |
| 127 | 0.0\% | 100.0\% | 127 | 0.0\% | 100.0\% |
| 128 | 0.0\% | 100.0\% | 128 | 0.0\% | 100.0\% |


| 129 | 0.0\% | 100.0\% | 129 | 0.0\% | 100.0\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 130 | 0.0\% | 100.0\% | 130 | 0.0\% | 100.0\% |
| 131 | 0.0\% | 100.0\% | 131 | 0.0\% | 100.0\% |
| 132 | 0.0\% | 100.0\% | 132 | 0.0\% | 100.0\% |
| 133 | 0.0\% | 100.0\% | 133 | 0.0\% | 100.0\% |
| 134 | 0.0\% | 100.0\% | 134 | 0.0\% | 100.0\% |
| 135 | 0.0\% | 100.0\% | 135 | 0.0\% | 100.0\% |
| 136 | 0.0\% | 100.0\% | 136 | 0.0\% | 100.0\% |
| 137 | 0.0\% | 100.0\% | 137 | 0.0\% | 100.0\% |
| 138 | 0.0\% | 100.0\% | 138 | 0.0\% | 100.0\% |
| 139 | 0.0\% | 100.0\% | 139 | 0.0\% | 100.0\% |
| 140 | 0.0\% | 100.0\% | 140 | 0.0\% | 100.0\% |
| 141 | 0.0\% | 100.0\% | 141 | 0.0\% | 100.0\% |
| 142 | 0.0\% | 100.0\% | 142 | 0.0\% | 100.0\% |
| 143 | 0.0\% | 100.0\% | 143 | 0.0\% | 100.0\% |
| 144 | 0.0\% | 100.0\% | 144 | 0.0\% | 100.0\% |
| 145 | 0.0\% | 100.0\% | 145 | 0.0\% | 100.0\% |
| 146 | 0.0\% | 100.0\% | 146 | 0.0\% | 100.0\% |
| 147 | 0.0\% | 100.0\% | 147 | 0.0\% | 100.0\% |
| 148 | 0.0\% | 100.0\% | 148 | 0.0\% | 100.0\% |
| 149 | 0.0\% | 100.0\% | 149 | 0.0\% | 100.0\% |
| 150 | 0.0\% | 100.0\% | 150 | 0.0\% | 100.0\% |


[^0]:    ${ }^{1}$ The intersection was projected to meet mobility standards during the Reedsport TSP horizon year (2025). The intersection was analyzed using HCM 2000 methodologies. The future conditions analysis utilizes HCM $6^{\text {th }}$ edition.

